V. CONCLUSION

The introduction of [I] claims that the "generalized" error, i.e., the $y - \hat{y}$ of this note, which is defined in [1, eq. (2.5)], converges to zero despite any initial parameter or state error regardless of input sequence or the magnitude of the constant adaptation gains. The counterexample of the preceding section disproves this claim. Furthermore, the PRBS used in the simulated failure to force the plant and identifier should provide the necessary richness requirements evoked in **[I]** for consistent parameter estimate convergence, thereby also belying that claim.

Presently the **stall** failure discussed in **this** note of the parallel **MRAS** with adaptive error filtering of **[I]** appears to be infrequent, but unpredictable. The only apparent conclusion is that a plant with poles near the unit circle in combinatiop with an erratically converging identifier is most likely to generate $\hat{A}(z, k)$ root migration outside the unit circle, possibly leading to matching $\hat{C}(z, k)$ roots and identifier stall. Clearly, further study is required to firmly delineate the applicability of output error identifiers such **as** in **[I],** [4], and [5] since, unfortunately, a claim of desirable behavior, i.e., $\hat{y} \rightarrow y$, apparently does not proceed solely from the proof of "processed generalized" error decay to zero, i.e., $s(k) \rightarrow 0$ as $k\rightarrow\infty$.

REFERENCES

- **I. D.** Landau, **"Elimination of the real positivity** condition **in the design of parallel**
- MRAS," IEEE Trans. Automat. Contr., vol. AC-23, pp. 1015–1020, Dec. 1978.
— , "Unbiased recursive identification using model reference adaptive techniques,"
IEEE Trans. Automat. Contr., vol. AC-21, pp. 194–202, Apr. 1976, $[2]$ **dum to 'Unbiased recursive identification using model reference, adaptive techniques,'"** *IEEE Trans. Automat. Contr.***, vol. AC-23, pp. 97-99. Feb. 1978.**
- $[3]$ L. Dugard, I. D. Landau, and H. M. Silveira, "Adaptive state estimation using MRAS techniques: Convergence analysis and evaluation," Laboratoire d'Automa**tique de Grenoble, Grenoble, France, Note LAG** 79-06. **Mar.** 1979.
- $[4]$ **D. Parikh, S.** *C* **Sinha, and N.** Ahrned, "On **a modification of the SHARF algorichm,"**
- n Proc. 22nd Midwest Symp. Circuits and Syst., Philadelphia, PA, June 1979.
C. R. Johnson, Jr. and T. Taylor, "CHARF convergence studies," in Proc. 13th
Asilomar Conf. Circuits, Syst., Comput., Pacific Grove, CA, Nov. 1979 - 151
- [6]
- digital filter," Univ. Newcastle, Newcastle, Australia, Tech. Rep. EE7914, July 1979.
C. R. Johnson, Jr., "A convergence proof for a hyperstable adaptive recursive filter,"
IEEE Tr*ans. Inform. Theory*, vol. IT-25, pp. 745 $\overline{7}$

Instability of Optimal-Aim Control

B. **ROSS BARMISH** *AND* ARIE FEUER

Abstract-It is shown that the so-called optimal-aim control strategy [1] might destabilize a controllable linear time-invariant system. This raises a serious question about the efficacy of this strategy when applied to a more complicated nonlinear power system.

I. **INTRODUCIION**

In **[11,** a rather novel approach is described which is intended for regulation of a class of nonlinear systems. At each instant of time, **an** admissible control is chosen which *minimizes* the state-space angle **between** the **state** derivative and the **direction** of the equilibrium state. *On* the surface, such an approach appears to be an attractive alternative to the **usual** difficulties which one would encounter when applying classical **techniques.'** Delving a little below the surface, however, we find

ter, Rochester, *NY* 14627. **B. R Barmish is** with **the Department of Electrical Engineering, University of Roches-A. Feuer is** with Bell **Laboratories, Holmdel, NJ 03733.**

¹Infinite-dimensional function space optimizations are replaced by "simpler" finite-
dimensional state space optimizations. Furthermore, the approach easily accommodates state-dependent input constraints and model variations.

a number of fundamental difficulties associated with the stability properties of these so-called optimal-aim controls. It was demonstrated in [2] that instability might occur when using control strategies (see [3]) which are **similar** in spirit to the optimal-aim strategy of [I]. Strictly **speaking,** however, the instability theorem of *[2]* does *nor* apply to the controllers of [**112** (see [4] and [5D. Nevertheless, we shall **see** in the sequel that the optimal-aim control strategy might indeed induce instability in the case of **[I]** as well.

We shall present two counterexamples to the conjectured stability. In our first counterexample, an asymptotically stable linear time-invariant system is rendered unstable via application of optimal-aim **control.** In our second counterexample, we examine an unstable linear time-invariant system which is stabilizable via linear feedback [6]. When optimal-aim control is applied in lieu of linear feedback, the system becomes unstable.

11. BRIEF REVIEW OF OPTIMAL AIMING

This control procedure **(see** [l] for full details) is developed for nonlinear regulation systems having additive linear control structures, i.e., we consider a system of state equations of the form

$$
\begin{aligned}\n\dot{x}(t) &= f(x(t)) + Bu(t), & t > 0, \, x(t) \in R^n \\
(t) & \in U = \{ \omega \in R^m : \omega_j \in [\omega_{j0}, \omega_{jl}], & j &= 1, 2, \cdots, m \}\n\end{aligned}
$$

with $f(\sigma_c)=0$ and $B'B = diag(C_i)$, $C_i > 0.3$ It is implicitly assumed that $f(\cdot)$ is "sufficiently regular" to guarantee the existence and uniqueness of solutions.

Following the notation in [1], we define the set $\Delta(x(t)) \stackrel{\triangle}{=} {\delta \in R^n : \delta}$ $f(x(t)) + B\omega$: $\omega \in U$ of *achievable derivatives* at the state $x(t)$ and the *reference vector* $\rho(x(t)) \triangleq \sigma_c - x(t)$. $(\sigma_c$ is the desired equilibrium.) The angle between $\delta \in \Delta$ and $\rho \in R^n$ is then given by

$$
\theta(\delta,\rho) = \begin{cases}\n0 & \text{for } \delta = 0 \text{ and } \rho \neq 0 \\
\cos^{-1}\left[\frac{\delta'\rho}{\|\delta\| \|\rho\|}\right] \in [0,\pi] & \text{for } \delta \neq 0 \text{ and } \rho \neq 0 \\
\frac{\pi}{2} & \text{for } \rho = 0\n\end{cases}
$$

where $\|\cdot\|$ is the usual Euclidean norm.

termed **on** *optimal aimpair* **if,** at each instant of *time I,* we have4 Within this framework, a control $u(\cdot)$ and trajectory mate $x(\cdot)$ are

$$
\theta(\dot{x},\rho) = \min_{\delta \in \Lambda} \theta(\delta,\rho)
$$

and either

u

$$
\|\dot{x}\| = \max_{\delta \in \Delta} \|\delta\| \quad \text{for } \theta(\dot{x}, \rho) < \frac{\pi}{2}
$$

$$
\theta(\delta, \rho) = \theta(\dot{x}, \rho)
$$

or

$$
\|\dot{x}\| = \min_{\delta \in \Delta} \|\delta\| \quad \text{for } \theta(\dot{x}, \rho) > \frac{\pi}{2}
$$

$$
\theta(\delta, \pi) = \theta(\dot{x}, \rho)
$$

Finally, the control $u(\cdot)$ giving rise to the minimum of $\theta(\dot{x}, \rho)$ is called an *optimal-aim control.*

precise, *i(r)* **should be interpreted as a right-hand derivative** (%e **[ID.** 4 To simplify notation, the dependence on t and $x(t)$ has been suppressed. To be

Department of Energy. Manuscript reseived October *29,* 1979. This **work was supported in part by the US.**

satisfy the preconditions of the theorem in 121. 2The possible nondifferentiable character of the control **law does not enable us to**

maaix above to be consistent with the notation in [I]. 3The analysis to follow wil **also be valid if** *B* **is a full rank matrix. We use the diagonal**

111. COUNTEREXAMPLES **TO CONTECTURED STABILITY**

For **our** first example, we consider a **linear** time-invariant system described by

$$
\begin{aligned}\n\dot{x}_1(t) &= x_1(t) - \xi x_2(t) \\
\dot{x}_2(t) &= 2x_1(t) - 2x_2(t) + u(t); \quad t > 0\n\end{aligned}\n\tag{S_1}
$$

with control restraint $|u(t)| \leq M(M>0)$ (ξ is a constant parameter).

To begin our analysis, we first note that this system (with $u(t) \equiv 0$) has a characteristic polynomial $p(\lambda) = \lambda^2 + \lambda + (2\xi - 2)$. Hence, this system is

stable (also controllable) for all $\xi > 1$. Now, we have the following result. *Theorem: Consider the system* (S_1) *with control restraint* $|u(t)| < M$ *and parameter* $\xi > 1$ *fixed. Then this system is unstable when subjected to an optimal-aim control strategy.*

Proof: Our proof will be accomplished by constructing a number $r>0$ and a set Ω , having the following properties:

1) $[0 \ 0]' \in \Omega$, (note that here σ _c = $[0 \ 0]'$) and

2) for every initial state $x(0) \in \Omega_r$, $x(0) \neq [0 \ 0]$, there exists a time $T>0$ such that in the resulting "optimal-aim trajectory," $x(t)$ satisfies

$$
||x(T)||=r.
$$

To accomplish 1) and 2), we first choose $r > 0$ so that

$$
r \leqslant \frac{M}{3} \, . \tag{1}
$$

Next we define

$$
\Omega_r \stackrel{\scriptscriptstyle \Delta}{=} \left\{ \begin{bmatrix} x_1 & x_2 \end{bmatrix} \in \mathbb{R}^2; \qquad x_1 \geq (\xi + \epsilon) x_2, x_2 \geq 0, \|x\| < r \right\} \tag{2}
$$

where **e** is fixed *so* that

$$
0 < \epsilon < 1. \tag{3}
$$

Clearly, Ω , as defined in (2) has property 1), namely, $[0 \ 0] \in \Omega$. To prove property 2), let us define two angle mappings $\theta_+(\cdot, \cdot)$ and $\theta_-(\cdot, \cdot)$ **on** the set *0,* by

$$
\theta_{+}(x_1, x_2) \stackrel{\triangle}{=} \pi + \tan^{-1} \frac{x_2}{x_1} - \tan^{-1} \frac{M + 2(x_1 - x_2)}{x_1 - \xi x_2}
$$
(4a)

$$
\theta_{-}(x_1, x_2) \stackrel{\triangle}{=} \pi - \tan^{-1} \frac{x_2}{x_1} - \tan^{-1} \frac{M - 2(x_1 - x_2)}{x_1 - \xi x_2}.
$$
 (4b)

In the sequel, the following facts and observation will be useful.

1) All angles above, by convention, take values in $[0, \pi]$.

2) By (1) and (2), if $[x_1 \ x_2]^r \in \Omega_r$

$$
x_2 < \frac{M}{3(\xi+\epsilon)}.
$$

Hence, by (3)

$$
x_2 < \frac{M}{3\xi}.
$$
 (5)

3) By (1) and (2), if $[x_1 \ x_2]^r \in \Omega$,

$$
2(x_1 - x_2) < 2x_1 < 2r < \frac{2}{3}M < M. \tag{6}
$$

4) If the current state is $x(t)=[x_1 \ x_2]^t \in \Omega_r$, then $\theta_+(x_1, x_2)$ is the state-space angle between the reference vector and $x(t)$ which results upon application of full positive control $u(t) = +M$. Similarly, $\theta_-(x_1, x_2)$ summarizes the effect of full negative control $u(t) = -M$.

5) If $x(t) = [x_1 \ x_2] \in \Omega_r$, then the optimal-aim control strategy dictates that either $u(t) = +M$ or $u(t) = -M$, i.e., any intermediate control value $m \in [-M, M]$ will result in a state-space angle which exceeds either $\theta_{+}(x_1, x_2)$ or $\theta_{-}(x_1, x_2)$.

This is apparent from **(4)** with *M* replaced by *m* and **(9. (See** also Fig. $1.$

Fig. 1. The set Q,.

Facts 4) and 5) clearly imply that being in a state $x(t) = [x_1 \ x_2]^t \in \Omega_r$ **,** the control will be

$$
u = \begin{cases} +M & \text{if } \theta_+(x_1, x_2) - \theta_-(x_1, x_2) < 0 \\ -M & \text{if } \theta_+(x_1, x_2) - \theta_-(x_1, x_2) > 0.5 \end{cases}
$$
 (7)

Next we are going to show that whenever on the boundaries $x_1 = (\xi +$ On the boundary $x_1 = (\xi + \epsilon)x_2$, we have ϵ)*x*₂ or *x*₂ = 0 of Ω ,, the optimal aim trajectory is directed into Ω .

$$
\theta_{+}(x_1, x_2) - \theta_{-}(x_1, x_2) = 2 \tan^{-1} \frac{1}{\xi + \epsilon} + \tan^{-1} \frac{M - 2x_2(\xi + \epsilon - 1)}{\epsilon x_2} - \tan^{-1} \frac{M + 2x_2(\xi + \epsilon - 1)}{\epsilon x_2}.
$$

Using **(3)** and *(5),* we observe that

and

that

$$
\frac{1}{\xi+\epsilon} > \frac{1}{\xi+1}
$$

$$
2x_2(\xi+\epsilon-1)<\frac{2}{3}M.
$$

Using these two inequalities and the fact that $\tan^{-1}(\cdot)$ is a monotonicaUy increasing function of its argument, we get

$$
\theta_{+}(x_1, x_2) - \theta_{-}(x_1, x_2) > 2 \tan^{-1} \frac{1}{\xi + 1} + \tan^{-1} \frac{M}{3\epsilon x_2} - \tan^{-1} \frac{5M}{3\epsilon x_2}
$$

(using standard trigonometrical identities)

 \sim

$$
= \tan^{-1} \frac{2(\xi+1)}{\xi(\xi+2)} - \tan^{-1} \frac{12\epsilon x_2 M}{9\epsilon^2 x_2^2 + 5M^2}
$$

>
$$
\tan^{-1} \frac{2(\xi+1)}{\xi(\xi+2)} - \tan^{-1} \frac{4}{5\xi} \Biggl(\text{recall } x_2 < \frac{M}{3\xi} \Biggr).
$$

Again we use the monotonicity of $\tan^{-1}(\cdot)$ and note that for $\epsilon > 1$

$$
\frac{2(\xi+1)}{\xi(\xi+2)}>\frac{4}{5\xi}.
$$

Hence, we conclude that

$$
\theta_{+}(x_1, x_2) - \theta_{-}(x_1, x_2) > 0
$$

for $x_1 = (\xi + \epsilon)x_2$. Hence, by (7), $u = -M$. Now, by (6), $\dot{x}_2(t) = 2(x_1 - x_2) - M < 0$, which means that the trajectory is directed back into Ω . from the boundary $x_1 = (\xi + \epsilon)x_2$ (note that $x_1(t) = x_1 - \xi x_2 > 0$). On the other boundary $x_2 = 0$, we have

$$
16.8
$$

$$
\theta_+(x_1, x_2) - \theta_-(x_1, x_2) = \tan^{-1}\frac{M-2x_1}{x_1} - \tan^{-1}\frac{M+2x_1}{x_1} < 0.
$$

⁵Equality implies $u = -M$. This can be seen by noting that for $[x_1 \ x_2] \in \Omega_r$, $\theta(x, \rho) > \pi/2$. Hence, this choice of u will achieve the required minimum as defined by the **"optimal-aim control"**

Fig. 2. Sample **trajectories** for Example 1 $(M=1 \text{ and } \xi=2)$.

Then by (7), $u=M$ and $\dot{x}_2(t)=2(x_1-x_2)+M>0$. Once again, the trajectory is directed from the boundary $x_2 = 0$ back into Ω_r .

Up to **this** point, we have **shown** that the only way an "optimal-aim trajectory" can escape from Ω , is through its boundary $||x|| = r$. Next, we are going to show that every such trajectory does, in fact, *cross* this boundary in finite time.

We have from (S_1)

$$
\dot{x}_1(t) = x_1(t) - \xi x_2(t).
$$

Hence, if $x(t) \in \Omega$, then by (2), it follows that $x_1(t) \ge (\xi + \epsilon) x_2(t)$ or, equivalently,

$$
x_2(t) \leq \frac{1}{\xi+\epsilon} x_1(t).
$$

Then

$$
\dot{x}_1(t) \ge x_1(t) - \frac{1}{\xi + \epsilon} \xi x_1(t) = \frac{\epsilon}{\xi + \epsilon} x_1(t)
$$

or

$$
x_1(t) > x_1(0) e^{(\epsilon/(\xi + \epsilon))t}
$$

which means that $||x(T)|| = r$ for some $0 < T < (\xi + \epsilon/\epsilon) \ln(r/x_1(0))$. So we **see** that For any initial condition, even if arbitrarily close to the origin, we cannot avoid future states having norm $r = M/3$ or larger. This enables **us** to conclude that the system is unstable and the theorem is proved. \square

Remark: It is of interest to note that, contrary to our expectation, one is *mr* able to do better with more available control effort. With larger *M,* we do, in fact, worse. The relation **between** *r* and *M* (from (1) it follows that we may choose $r=M/3$) and the proof of the theorem reveals the following. The larger *M,* the further away from the origin **certain** trajectories will be forced to go by the optimal aim control.

In Fig. *2,* sample trajectories are indicated corresponding to *M=* 1 and $\xi = 2$. Clearly, these trajectories are approaching a point and the distance of this point from the origin grows with *M.*

For our second counterexample, we consider a linear time-invariant system described by

$$
\dot{x}_1(t) = x_1(t) + x_2(t) \n\dot{x}_2(t) = x_2(t) + u(t); \quad t > 0
$$
\n(5₂)

with control restraint $-M \le u(t) \le 2M(M>0)$.

To **begin,** we note that this system *can* easily be stabilized **using** linear feedback.⁶ Using optimal-aim control instead, we encounter difficulties.

Using the angles $\theta_+(x_1, x_2)$ and $\theta_-(x_1, x_2)$ as in the proof of Theo**rem 1,** the following fact is readily established. Any optimal-aim trajectory $x(\cdot)$ which begins in the set

$$
\Omega_{+} = \{ (x_1, x_2) \in R^2; \quad x_1 \ge 0, x_2 \ge 0 \}
$$

remains *forever* within this set. Consequently, if $x(0) \in \Omega_+$, it follows that $\dot{x}_1(t) > x_1(t)$ (since $x_2(t) \ge 0$). Hence, $x_1(t) \ge e^t x_1(0)$ and we see this system is unstable. Hence, for **this** system, the optimal-aim control would not **be** desirable.

Iv. CONCLUSION

Given the Fact that comprehensive global stability criteria do not exist for arbitrary complex nonlinear systems, it is unreasonable **(unfair)** to judge the efficacy of a given control law in terms of its ability to provide an *u priori* guarantee of stability. Nevertheless, it is Felt that any *sound* control strategy for nonlinear stabilization should **satisfy** the following **necessary** condition. Namely, when the strategy is specialized to a controllable linear time-invariant system, asymptotic stability should be assured. The optimal-aim control does not satisfy this necessary condition.

ACKNOWLEDGMENT

The authors express their thanks to Reviewer *2* whose detailed **re**marks were quite helpful in improving the manuscript.

REFERENCES

- **111 R D. Barnard "An optimal-aim conpol strategy for** nonlinear **regulation-sytu"**
- **I21** IEEE Trans. Automat. Contr., vol. AC-20, pp. 200-208, 1975.
B. R. Barmish, R. J. Thomas, and Y. H. Lin, "Convergence properties of a class of **pointwise** control **swtepies,"** *IEEE Tram. Auromr. Conrr.,* **vol. AC-23, pp. 954-956, 1978.**
- **131** R **D. Barnard, "Continuous time implementation of optimal-aim** control," *IEEE Tram. Auromt. Conrr.,* **vol. AC-21, pp. 432-434, 1976.**
- **141 gies.'" IEEE Trans. Automat. Contragence properties of a class of pointwise control strate-
gies.'" IEEE Trans. Automat. Contr., vol. AC-24, pp. 673-674, 1979.**
- **151 vol. AC-24, pp. 674-675, 1979.** B. R. Barmish and R. J. Thomas, "Authors' reply," *IEEE Trans. Automat. Contr.*,
- **If4** *^C***T.** *Chen, Inrroducrion 10 Linetv @stem Theory.* New **York: Holt, Rinehart and Winston. 1970.**

Further Comments on "On the Numerical Solution of the Discrete Time Algebraic Riccati Equation"

ALAN J. LAUB

The purpose of **this** note is **to** make a few brief comments on [l] which, in turn, comments on [2]. It is unfortunate that the authors of [1] were unaware of the existence of **[2],** which is based on the Bachelor's degree thesis of Pappas [3]. Moreover, to set he historical record straight, the basic idea of the generalized eigenvalue problem formulation upon which *[2]* and [3] were based appeared as Appendix **1** of [4] **@p. 47-48),** a **report** which **achieved wide** (although apparently not **wide** enough) circulation.

The authors **of [I]** claim that *[2]* does not address the issue **OF** degeneracy. That claim is, of course, false **as** the proof (actually, it is almost a parenthetical remark) appears very clearly in the first paragraph of the proof of Theorem **4** in *[2].*

Several interesting points are raised in [1], particularly the formulation of the problem which avoids G_2^{-1} . This can be potentially a very important reformulation if G_2 is badly conditioned with respect to inversion. A thorough discussion of this and related questions appears in a fine paper of Van Dooren *[5].*

⁻ *M* < **u(r)** < **2** *M.* **we simply use a %-called** *sarurm'on linear feedhck.* **61~ is controllable; its poles** *can* **be assigned arbitrarily. To accommodate the bound**

Manuscript received August 1 I, 1980

The author is with **the Department of Electrical Engineering-Systems, University of Southern** *California* **Los Angeles,** *CA* **90007.**