

#### Levi Schächter

Department of Electrical Engineering Technion - Israel Institute of Technology Haifa 32000, ISRAEL



- Constraints on optical structures
- Optical structures
- Four acceleration configurations
- Comments on luminosity & power

#### **Constraints**

- Gradient: order of 1[GV/m] or higher.
- ◆ Efficiency: limited by radiation source and acceleration scheme # Lasers anticipated efficiency of wall-plug to light 10% → 30%?!
   # Efficiency of acceleration scheme – major difficulty
- Breakdown: at optical wavelengths dielectrics sustain higher fields comparing to metals.
- Manufacturing constraints favor planar structures consistent with luminosity constraints.
- **Single Mode**: width of vacuum tunnel  $0.3\lambda 0.8\lambda$
- Machining tolerance: 1µm at 3 cm wavelength. Four orders of magnitude difference difficult to be preserved at λ=1µm (poster).





#### Structure parameters



**Configurations** 





#### •Wake parameter:

Decelerating field for a given charge .....  $E_{dec} \equiv \kappa q$ •*Beam-loading parameter*:  $\kappa = 2 / 4\pi \varepsilon_0 R^2$ 

Beam-loading of the accelerating mode .....  $E_{dec}^{(F)} \equiv \kappa_1 q$ 



Contribution of the fundamental to the total deceleration

Stupakov & Bane, PR STAB, 2003

External Laser

> Traveling-wave Acceleration Module



# Single bunch & no feedback

• Loaded gradient:  $E_{\text{eff}} \equiv E_{\text{acc}}$ 

$$E_{\rm eff} \equiv E_{\rm acc} - E_{\rm dec} = E_{\rm acc} - \kappa q$$

External Laser Traveling-wave Acceleration Module

Zero force charge

• EM energy:

• Kinetic energy:

$$U_{\rm EM} \equiv P_{\rm Laser} \frac{d}{V_{\rm gr}} (1 - V_{\rm gr} / c)$$

 $\Delta U_{\rm KIN} \equiv q E_{\rm eff} d$ 

$$= \frac{\Delta U_{\text{KIN}}}{U_{\text{EM}}} = \eta_{\text{max}} \frac{4q(q_0 - q)}{q_0^2} \Rightarrow q_{\text{opt}} = \frac{1}{2}q_0 \equiv \frac{1}{2}\frac{E_{\text{acc}}}{\kappa}$$

Maximum efficiency is set by the projection of the <u>total deceleration on the fundamental !!</u>

K

 $\eta_{\rm max}$ 

## Single bunch & no feedback

Transverse PBG	Longitudinal PBG			
$R_{int} \approx 0.68\lambda$ $\varepsilon = 2.1, \ \lambda \approx 1.0 [\mu m]$ $Z_{int} \approx 19.5 [\Omega]$ $\beta_{gr} \approx 0.58$ $E_{max} \approx 2 [GV/m]$ $F_{Laser} \approx 50 [kW]$ $\eta \approx 6\%$ $q_{opt} \approx 7 \times 10^{4} e$ $E_{acc} \approx 1 [GV/m]$	$D_{int} \approx 0.55\lambda$ $\varepsilon = 2.1$ $\lambda \approx 1.5 [\mu m]$ $Z_{int} \Delta_{y} / \lambda \approx 250 [\Omega]$ $\beta_{gr} \approx 0.2$ $E_{max} \approx 2 [GV/m]$ $P_{Laser} \approx 2.3 [kW/\mu m]$ $\eta \approx 36\%$ $\overline{q}_{opt} \approx 5 \times 10^{4} [e/\mu m]$ $E_{acc} \approx 0.6 [GV/m]$ $B. Cowan, PR STAB, 2003$			
$\begin{array}{l} Cylindrical Bragg Structure \\ R_{int} &= 0.68\lambda \\ \varepsilon_1 &= 2.1, \varepsilon_2 &= 4 \\ \lambda &= 1[\mu m] \\ Z_{int} &= 56.4[\Omega] \\ \beta_{gr} &= 0.58 \\ E_{max} &= 2[GV/m] \end{array} \xrightarrow{P_{Laser}} = 18[kW] \\ \eta &= 9\% \\ \eta_{opt} &= 7 \times 10^4 e \\ E_{acc} &= 1[GV/m] \end{array}$	<b>Planar Bragg Structure</b> $D_{int} \approx 0.55\lambda$ $\varepsilon_{1} = 2.1, \varepsilon_{2} = 4$ $\lambda \approx 1[\mu m]$ $Z_{int}\Delta_{y}/\lambda \approx 57[\Omega]$ $\beta_{gr} \approx 0.48$ $E_{max} \approx 2[GV/m]$ $P_{Laser} \approx 5.3[kW/\mu m]$ $\eta \approx 8\%$ $q_{opt} \approx 3.3 \times 10^{4} [e/\mu m]$ $E_{acc} \approx 0.56[GV/m]$			

### Single bunch & no feedback



Maximum efficiency is set by the projection of the total deceleration on the fundamental



By splitting the bunch into a train of micro-bunches, the projection of the wake on the fundamental remains the same, but higher frequencies are suppressed

$$P(M) = q^{2}c\kappa\sum_{n=1}^{M}W_{n}\left[\frac{\operatorname{sinc}\left(\pi M\frac{\omega_{n}}{\omega_{1}}\right)}{\operatorname{sinc}\left(\pi\frac{\omega_{n}}{\omega_{1}}\right)}\right]^{2} = q^{2}c\,\overline{\kappa}(M)$$

$$= q^{2}c\,\overline{\kappa}(M)$$

$$0.8$$

$$0.6$$

$$0.4$$

$$0.2$$

$$0.2$$

$$0.2$$

$$0.2$$

$$0.0$$

$$0.2$$

$$0.0$$

$$0.4$$

$$0.2$$

$$0.2$$

$$0.0$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.2$$

$$0.0$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.4$$

$$0.2$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$

$$0.4$$



Train of bunches & no feedback

What is the efficiency in case of a train of micro-bunches?
For an answer, one needs to make two observations:

a) The laser pulse duration ought to be longer in order to account for the macro-bunch length.
b) The envelope of the laser pulse must be tapered, in order to compensate for beam loading.

External

Traveling-wave Acceleration Module

Laser



External

Traveling-wave Acceleration Module

Laser

Laser *tapered pulse* necessary to *compensate* for the beam loading in order to ensure *uniform* acceleration of *all* micro-bunches



**Train of bunches & no feedback**  

$$\eta = \frac{\left[12\left(1-\beta_{gr}\right)\frac{\kappa_{1}}{\kappa}\right]q(q_{0}-q)}{3\left[q_{0}-q+q\frac{\kappa_{1}}{\kappa}\left(\frac{1}{M}+1\right)\right]^{2}+\left[q\frac{1}{\beta_{gr}}\frac{\kappa_{1}}{\kappa}\right]^{2}}$$

$$\eta_{max} \approx 12\left(1-\beta_{gr}\right)\beta_{gr}^{2}\frac{\xi\left(1-\xi\right)}{\xi^{2}+3\beta_{gr}^{2}}$$

$$\eta_{max} \approx 12\left(1-\beta_{gr}\right)\beta_{gr}^{2}\frac{\xi\left(1-\xi\right)}{\xi^{2}+3\beta_{gr}^{2}}$$

$$q_{opt} \approx 3q_{0}\beta_{gr}^{2}\left[\sqrt{1+\frac{1}{3\beta_{gr}^{2}}}-1\right] = q_{0}\xi$$

$$M \gg 1, \frac{\kappa_{1}}{\kappa} \approx 1$$
In spite of splitting the macro-  
bunch, there still is 50% waste of  
the laser energy  $\Rightarrow$  feedback floop.

## Single bunch & feedback

- External laser field:  $E_{\rm L}$
- Input to acceleration module :  $E_{in} = E_L + E_{FB}$
- Output of the acceleration module :  $E_{\text{out}} = E_{\text{in}} \vec{E}_{\text{w}}$
- Feedback loop:  $E_{\rm FB} = \Gamma E_{\rm out}$

• Dynamics:



Fundamental

mode

External Laser

> Traveling-wave Acceleration Module

> > Active Medium

 $2\kappa_1 q$ 

$$E_{\text{out}}(t) = \Gamma E_{\text{out}}(t - T_{rr}) + E_L(t - d/c\beta_{\text{gr}}) - E_W^{(F)}(t - d/c\beta_{\text{gr}})$$

 $1 - e^{-2\psi} = 1/Q$ 

 $\prod_{\text{overall gain}} = \underbrace{g}_{\text{gain loss coefficient}} \underbrace{e^{-\psi}}_{\text{gain loss coefficient}}$ 

Single bunch & feedback



• External energy injected into the system:

$$U_{\text{Laser}} = \frac{\left(E_L \lambda\right)^2}{Z_{\text{int}}} \tau_{\text{EM}} \quad , \quad U_{\text{ACTIVE}} = \left(g^2 - 1\right) U_{\text{OUT}} = \left(g^2 - 1\right) \frac{\left[\lambda \left(E_{\text{acc}} - 2\kappa_1 q\right)\right]^2}{Z_{\text{int}}} \tau_{\text{EM}}$$

• In steady state it compensates energy which leaves:  $\Delta U_{\text{KIN}}$  and  $U_{\text{LOSS}} = U_{\text{OUT}}/Q$  $\eta = \frac{\Delta U_{KIN}}{U_{LASER} + U_{ACTIVE}} = \frac{\Delta U_{KIN}}{\Delta U_{KIN} + U_{LOSS}} = \frac{1}{1 + \frac{1}{Q} \frac{U_{OUT}}{\Delta U_{KIN}}}$ 

$$q_{\text{opt}} = \frac{1}{2}q_0, \quad \eta_{\text{max}} \simeq \frac{1}{1 + \frac{1}{Q\frac{\kappa_1}{\kappa}}} \simeq \begin{cases} 1 & Q \gg 1\\ \frac{\kappa_1}{\kappa} & Q \to 1 \end{cases}$$

High efficiency but,

small number of electrons → train of bunches and feedback loop

### Train of bunches & feedback



Ensure that output & feedback are consistent with the necessary input !!









#### Fluence

	NLC	Single no FB	Single no FB	Train & FB	Train & FB	
f <sub>rr</sub> [Hz]	120	1(6)	1(9)	1(6)	1(6)	り着
N <sub>micro</sub>	190	1	1	1(3)	1(3)	
N <sub>el</sub>	0.75(10)	5(4)	5(4)	1(6)	1(6)	
σ <sub>z</sub> [nm] =	0.11(6)	4	4	4	4 <i>De</i>	nsity !
σ <sub>x</sub> [nm]	245	245	24.5	245	24.5	
σ <sub>y</sub> [nm]	2.7	2.7	0.27	2.7	0.27	
n <sup>-1/3</sup> [Å]	2.1	3.8	0.8	1.4	0.3	
H <sub>D</sub>	1.4	1.0	1.0	1.0	1.0	
L[cm <sup>-2</sup> sec <sup>-1</sup> ]	2(34)	3(25)	3(30)	1.2(34)	1.2(36)	
Beam power [MW]	13.7	4(-3)	4	80	80	

#### Summary: Dielectric Structures



# Summary: Configurations



# Summary: Efficiency & Luminosity



Amplifier compensates for all **radiation loss** (active enhancement of the Q—factor) facilitated by the wake being "quasi-coherent"

(II) External laser compensates for **beam-loading** (tapered pulse)

(III) Luminosity

(I)

Talk in Exotic schemes WG