

# Spectro-Temporal Imaging of Optical Pulses With a Single Time Lens

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**Abstract**—Spectro-temporal imaging (*time-to-frequency conversion*) constitutes a simple and direct (*single-shot*) technique for the high-resolution measurement of fast optical temporal waveforms. Here, we experimentally demonstrate that spectro-temporal imaging of an optical pulse can be achieved with a *single* time lens (quadratic phase modulator) operating under the appropriate conditions. As compared with the conventional solution, our proposal avoids the use of an input dispersive device preceding the time lens, thus, representing a much simpler and more practical alternative for implementing spectro-temporal imaging.

**Index Terms**—Optical pulse propagation, optical pulse shaping, pulse characterization, ultrafast optics.

SPACE–TIME duality is based on the analogy between the equations that describe the paraxial diffraction of beams in space and the first-order temporal dispersion of optical pulses in a dielectric [1]–[7]. The duality can also be extended to consider imaging lenses: The use of quadratic phase modulation on a temporal waveform is analogous to the action of a thin lens on the transverse profile of a spatial beam [1]–[6]. The time lens can be practically implemented using an electrooptic phase modulator driven by a sinusoidal radio-frequency (RF) signal [2], [4], [5], by mixing the original pulse with a chirped pulse in a nonlinear crystal (sum-frequency generation) [3], or by means of cross-phase modulation of the original pulse with an intense pump pulse in a nonlinear fiber [6]. Optical signal processing operations based on time lens include real-time Fourier transformation [1], [5], temporal imaging [2], [3], and spectro-temporal imaging (time-to-frequency conversion) [4]–[6]. Here we investigate a new regime in the interaction between optical pulses and time lenses. In particular, we demonstrate that when a time lens operates on an optical pulse, this pulse can enter a regime where the input pulse amplitude is mapped from the time domain into the frequency domain (time-to-frequency conversion). As schematically shown in Fig. 1, this regime can be interpreted as the *frequency-domain* dual of the temporal Fraunhofer regime (frequency-to-time conversion or real-time Fourier transformation by temporal dispersion [7]), and as a result, we will refer to it as *spectral* Fraunhofer regime. In this letter, we derive the conditions for

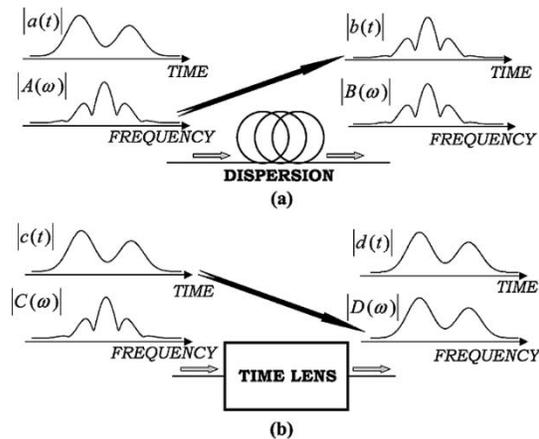


Fig. 1. Dual Fraunhofer regimes: (a) frequency-to-time conversion using dispersion and (b) time-to-frequency conversion using a single time lens.

achieving time-to-frequency conversion using a single time lens as well as the expressions governing this operation. We also provide an experimental demonstration of the phenomenon using an electrooptic time lens. Among other potential applications, spectro-temporal imaging can be applied for the measurement of the intensity temporal profile of ultrashort optical pulses using a spectrum analyzer. In contrast with other approaches, this method provides a fast, direct (*single-shot*), and unambiguous measurement of the temporal waveform.

Spectro-temporal imaging has been previously demonstrated using a spectral compressor, i.e., a system comprising a time lens preceded by a dispersive device in the appropriate balance [4]–[6]. As a main advantage, our proposal (using a single time lens operating in the spectral Fraunhofer regime) simplifies the design and implementation of spectro-temporal imaging systems since it avoids the use of a dispersive device preceding the time lens. The concept of a temporal imaging system where the input signal is not dispersed before receiving the quadratic phase-shift has been previously proposed and demonstrated for the case of input *electrical* signals (see, for instance, [8] and [9]). The main difference between our present work and the previous art is that our input signal is optical (e.g., an optical pulse) instead of electrical. Obviously, this translates into a significantly different system implementation. Specifically, the time lens mechanism in the previous work was implemented by modulating the input electrical signal with a chirped optical pulse, which was, in turn, obtained by dispersing a transform-limited optical pulse in an appropriate section of single-mode optical fiber. This time lens operation is only suitable for processing electrical signals but, in principle, it cannot be used to process optical signals. For instance, in our experimental demonstration, we have implemented the time lens operation using an

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electrooptic phase modulator driven by a sinusoidal RF signal, which is a time lens mechanism suitable for processing optical pulses. We recall that the main contribution of our work is the formal derivation and experimental demonstration of the design specifications of a time lens to operate as a spectro-temporal imaging system (i.e., what we have called spectral Fraunhofer conditions).

First, we theoretically investigate the spectral Fraunhofer regime in a time lens. In what follows, the involved signals are assumed to be spectrally centered at the optical frequency  $\omega_0$ , we work with the complex temporal envelope of the signals, and we ignore the average delay introduced by the time lens. A time lens is a phase-only modulator with a phase modulation function [2]

$$m(t) = \exp(j\phi(t)) \propto \exp\left(j\left[\frac{\ddot{\phi}_t}{2}\right]t^2\right) \quad (1)$$

where  $\ddot{\phi}_t = [\partial^2\phi(t)/\partial t^2]_{t=0}$  is the phase factor of the time lens. Let us now evaluate the action of the time lens over a given *arbitrary* optical pulse  $c(t)$ . The output pulse  $d(t)$  from the time lens in response to the input pulse  $c(t)$  is given by  $d(t) = c(t)m(t)$ . In the frequency domain, the product can be described as a convolution  $D(\omega) = C(\omega) * M(\omega)$ , where  $D(\omega)$  and  $C(\omega)$  are the Fourier transforms of  $d(t)$  and  $c(t)$ , respectively, and  $M(\omega)$  is the Fourier transform of the time-lens modulation function,  $M(\omega) \propto \exp(-j[1/2\ddot{\phi}_t]\omega^2)$ . At this point, we note that since we are working with the complex temporal envelope of the signals, the variable  $\omega$  is the baseband frequency variable, i.e.,  $\omega = \omega_{\text{opt}} - \omega_0$ ,  $\omega_{\text{opt}}$  being the optical frequency variable. We derive that

$$\begin{aligned} D(\omega) &= C(\omega) * M(\omega) \propto \int_{\Delta\omega} C(\Omega) \exp\left(-j\left[\frac{1}{2\ddot{\phi}_t}\right][\omega - \Omega]^2\right) d\Omega \\ &\propto M(\omega) \int_{\Delta\omega} C(\Omega) \exp\left(-j\left[\frac{1}{2\ddot{\phi}_t}\right]\Omega^2\right) \exp\left(j\left[\frac{1}{\ddot{\phi}_t}\right]\omega\Omega\right) d\Omega \end{aligned} \quad (2)$$

where  $\Delta\omega$  is the total spectral bandwidth of the input pulse  $c(t)$  [ $\Delta\omega \ll \omega_0$ ] and the integration variable  $\Omega$  is a baseband frequency. If this bandwidth is sufficiently narrow so that

$$|\ddot{\phi}_t| \gg \frac{\Delta\omega^2}{8\pi} \quad (3)$$

then the phase term  $\exp(-j[1/2\ddot{\phi}_t]\Omega^2)$  within the last integral in (2) can be neglected, since  $|(1/2\ddot{\phi}_t)\Omega^2| < (1/2|\ddot{\phi}_t|)(\Delta\omega/2)^2 \ll \pi$ . In this case, (2) can be approximated by

$$D(\omega) \propto M(\omega) \int_{\Delta\omega} C(\Omega) \exp\left(j\left[\frac{1}{\ddot{\phi}_t}\right]\omega\Omega\right) d\Omega = M(\omega)c\left(t = \frac{\omega}{\ddot{\phi}_t}\right). \quad (4)$$

The last integral has been solved by considering  $\exp(j[1/\ddot{\phi}_t]\omega\Omega)$  as the *kernel* of a Fourier transformation. Equation (4) indicates that under the conditions of inequality (3) (*spectral Fraunhofer condition*), the spectrum of the output pulse  $D(\omega)$  is, within a phase factor  $[M(\omega)]$ , proportional to the input temporal waveform  $c(t)$ , evaluated at the instant  $t = \omega/\ddot{\phi}_t$ . In other words, the spectral energy distribution of

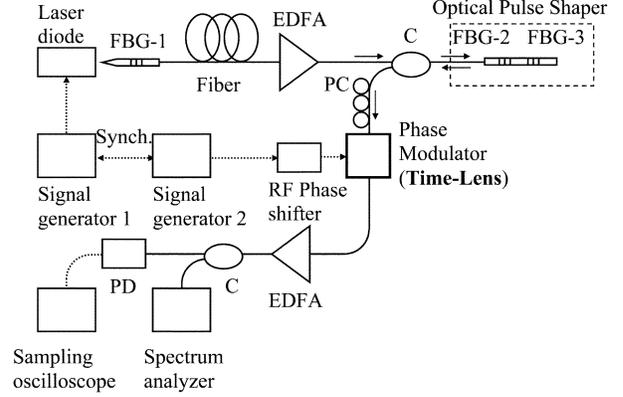


Fig. 2. Schematic of the experimental setup. Solid (dotted) lines are used for optical (electrical) signals. EDFA: Erbium-doped fiber amplifier. C: fiber coupler. PC: polarization controller. Synch.: synchronization.

the output optical pulse  $|D(\omega)|^2$  is an *image* of the temporal intensity distribution of the input optical pulse  $|c(t)|^2$ , i.e.,  $|D(\omega)|^2 \propto |c(t = \omega/\ddot{\phi}_t)|^2$  [see Fig. 1(b)]. The spectral Fraunhofer condition [inequality (3)] can be interpreted as a condition for the phase factor (chirp) of the time lens  $|\ddot{\phi}_t|$ , depending on the fastest temporal feature of the input optical signal to be measured  $\delta t \approx 2\pi/\Delta\omega$  (i.e., depending on the required temporal resolution  $\delta t$ ). Specifically, according to (3), the shorter (faster) the temporal feature to be resolved, the larger the phase factor of the time lens must be.

Fig. 2 shows a schematic of our experimental arrangement to observe the spectral Fraunhofer regime. An actively mode-locked laser diode with an external resonator based on a uniform fiber Bragg grating (FBG-1) was used as the optical pulse source. The source generated optical pulses at a repetition rate of 0.99 GHz centered at a wavelength of 1548 nm. The generated pulses were nontransform-limited (chirped) nearly Gaussian pulses. These pulses were subsequently compressed to a time-width of  $\approx 17.5$  ps using dispersion compensating fiber. The compressed pulses were conveniently reshaped by means of an FBG-based optical pulse shaper, consisting of two consecutive uniform FBGs (FBG-2 and FBG-3). In particular, the FBGs were specifically designed to generate a nonsymmetric double pulse [see Fig. 3(b)] from the input Gaussian pulses. The gratings FBG-2 and FBG-3 were written in a boron-doped photosensitive fiber by continuous-wave ultraviolet (UV) radiation ( $\lambda = 244$  nm) using the phase-mask technology. The FBGs were 0.3 mm long and were spaced apart by 0.3 mm. The measured reflectivities of the gratings were 5.3% and 4.8%, respectively. In order to obtain the desired temporal optical waveform [nonsymmetric double pulse, as shown in Fig. 3(b)], it was required to introduce a  $\pi$ -phase shift between the reflection coefficients corresponding to the two individual gratings, FBG-2 and FBG-3. For this purpose, the grating structure was conveniently processed using UV radiation after its fabrication (i.e., trimming process).

A  $\text{LiNbO}_3$  electrooptic modulator, driven by a sinusoidal RF modulation signal, was used as the time lens mechanism [2], [4], [5]. The modulation frequency and modulation index (amplitude) were fixed to  $\omega_m = 2\pi 9.9$  GHz  $\times$  rad and  $A = 2.4$  rad, respectively. With these values, the phase factor of the time lens can be estimated as  $|\ddot{\phi}_t| \approx A\omega_m^2 \approx 9286.27$  GHz<sup>2</sup>  $\times$  rad [2]. Note that the two RF signal generators used to drive

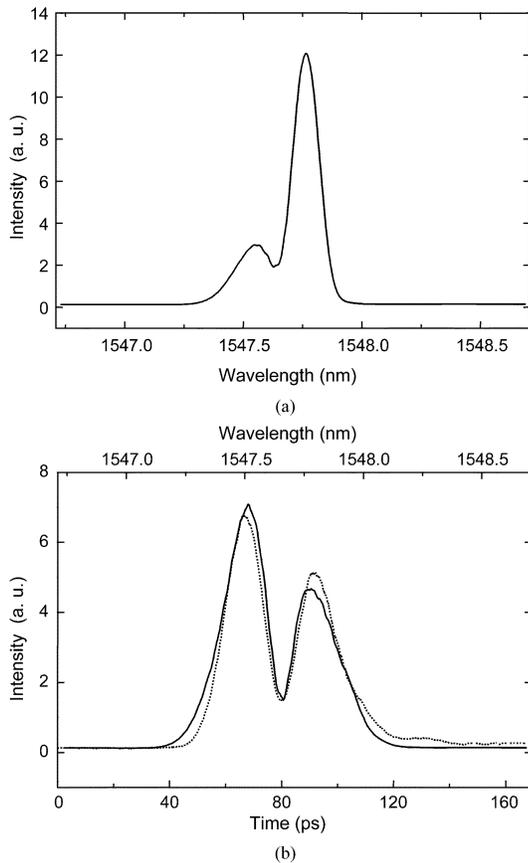


Fig. 3. Experimental results. (a) Measured spectrum of the input pulse to the time lens. (b) Measured spectrum of the output pulse from the time lens (solid curve, top scale) and measured temporal waveform of the input pulse to (output pulse from) the time lens (dotted curve, bottom scale).

the mode-locked laser diode and the electrooptic phase modulator (time-lens), respectively, were synchronized by means of a signal operating at 10 MHz. We also note that the required synchronization between the incoming optical pulses and the modulation RF signal in the time lens was ensured using an RF phase shifter. Finally, the optical signals were measured in the temporal domain using a fast photodetector (PD) followed by a sampling oscilloscope, both providing a bandwidth of  $\approx 50$  GHz. For their measurement in the spectral domain, we used a conventional optical spectrum analyzer providing a resolution of  $\delta\lambda \approx 0.015$  nm. Fig. 3(a) shows the measured energy spectrum of the input pulse (before the time lens). The total bandwidth of the input optical pulse is estimated to be  $\Delta\lambda \approx 0.5$  nm ( $\Delta\omega \approx 2\pi \times 62.5$  GHz  $\times$  rad). For the parameters used, the spectral Fraunhofer condition [(3)] is satisfied but in the form  $|\dot{\phi}_t| > \Delta\omega^2/8\pi$ . Fig. 3(b) (solid curve) shows the measured energy spectrum of the output pulse (after the time lens). For comparison, the measured temporal waveform of the input (output) pulse is also shown in Fig. 3(b) (dotted curve). The time and wavelength scales in Fig. 3(b) are related according to (4) by  $t-t_0 \approx -(2\pi c/\lambda_0^2 \dot{\phi}_t)(\lambda-\lambda_0)$ , where  $c$  is the speed of light in vacuum and  $t_0$  and  $\lambda_0$  are the central instant and wavelength of the optical pulse, respectively. Our experimental results confirmed our theoretical predictions. As expected, the energy spectrum of the optical pulse at the output of the time lens is an image of the temporal optical waveform at the input of the time lens, according to the relation given by (4). In other words, an effi-

cient spectro-temporal imaging process is achieved. Note that the sign of the time-to-frequency scale conversion is fixed by the sign of the phase factor  $\dot{\phi}_t$ , i.e., it depends on the half period that it is chosen for the modulation RF signal in the time lens. The observed deviations between the measured temporal waveform and the spectrum after modulation are associated with the following nonidealities in the system: 1) the spectral Fraunhofer condition (3) is not strictly satisfied, i.e., as mentioned above, it is satisfied as  $|\dot{\phi}_t| > \Delta\omega^2/8\pi$ ; and 2) the temporal duration of the input optical pulse ( $\approx 75$  ps) exceeds the time aperture  $\tau_a$  of the time lens ( $\tau_a \approx 1/\omega_m \approx 16$  ps [2]).

As previously mentioned, the temporal resolution provided by the spectro-temporal imaging system can be improved by increasing the magnitude of the phase factor  $|\dot{\phi}_t|$  [according to the spectral Fraunhofer condition in (3)]. In general, alternative technologies for implementing the time lens, such as those based on nonlinear processes [3], [6], allow achieving much larger phase factors than the electrooptic technology used herein and, consequently, have the potential for further improving the achievable temporal resolutions. As an example, a time lens such as that reported in [3] ( $\dot{\phi}_t \approx 6 \times 10^6$  GHz<sup>2</sup>  $\times$  rad) could be used to implement spectro-temporal imaging of optical pulses with a temporal resolution of order of a few hundreds of femtoseconds [as determined by the spectral Fraunhofer condition in (3)]. We note that this temporal resolution is similar to that reported in [3], where the temporal waveforms were measured using a temporal imaging system, i.e., using a configuration (dispersion + time lens + dispersion) much more complex than the one proposed herein.

In summary, we have demonstrated a new regime (spectral Fraunhofer regime) in the interaction between optical pulses and time lenses. In this regime, the temporal waveform of the input pulse is mapped into the spectral domain by the action of a time lens. Based on this idea, simplified spectro-temporal imaging systems, comprising a *single* time lens, can be implemented. These systems can be applied for measuring ultrafast temporal waveforms and we estimate that subpicosecond/femtosecond resolutions could be achieved using current technology.

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